Review Article

The Numerical Simulation of Properties with High Angular Speed & Low Angular Acceleration in Three & Five Freedoms of Robotic Arm I

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Abstract: In robot design and application the force and angle with angular speed is important so this study will model numerical simulation and discuss detail data to investigate their property. The force may increase as arm 1 angle increases whilst it may increase if angular speed increases in three freedoms. Meantime it will decrease if angular acceleration increases. It is found that with the angular speed increasing all three forces may increase whilst the angular acceleration will cause its increase too in five freedoms. From this value it is observed that F_2 is prior one to ensure the strength and fatigue life then F_2 is second one to estimate its strength whilst F_3 may be neglected. The force may increase as arm 1 angle increases whilst it may increase if angular speed increases in three freedoms. Meantime it will decrease if angular acceleration increases. There is big distance to attain 5KN between the conditions. The effective factor turn to the force is $F_1>F_3>F_2$ in three freedoms. The force may increase from 15N to 15KN and 18KN with F_3, F_2 and F_1 in five freedoms. Among them F_3 is the least one and F_1 is the biggest one. The effect factor turn is $F_1 >F_2 >F_3$. so the F_1 and F_2 is important one while F_3 is neglected.

Keywords: Numerical simulation; force and angle; angular speed & acceleration; robotic arm; angular Acceleration; three & five freedoms.

1. INTRODUCTION

In recent the robotic arm has been applied to many occasion in factory which can help people to work in difficult, dirty and dangerous place so its application will be more prevailed in future which is estimated in this study. China has been the largest country which can own the largest domestic market in the world, but it has the third market occupant since it has not owned the enough advanced condition [1-5]. So that we must positively construct the clean and criteria house to meet the demand for robotic arm to ensure precise work.

In robotic design the force is an important factor to consider since the strength must meet demand no matter what it may work in factory [6, 7]. So that according to the function it may be designed to satisfy the no fracture and longer fatigue life for its long life and high load to work in automatic flow line to be substituted to human worker. The biggest one will destination in this paper and how to save manufacture cost is the second one. So it is needed that the mass and load may become first thing to prepare; secondly for the cost decrease the redundant load shall be prohibited.

In this paper the condition is changed like angular speed and acceleration to observe the three forces status to ensure security of strength and save cost status. The three freedoms and five ones are investigated in this paper detail with parameters like force and angle with angular speed and acceleration. We try to find the various condition of effective factor in order to search intrinsic properties relationship which is the destination in this paper.

In short the properties are searched through parameters in detail. We look forward to finding new change with force and speed & acceleration for further research.

2. Numerical Simulations

In Figure 1 there are three freedoms in mechanical arm that name as 1~3. Meantime there are two other ones call 4&5which is included in five freedoms as a rotational and crawling function. In Figure 1 the schematic shows the simplified principle of robot. The coordinate XAY is three freedoms and X′A′Y it five freedoms. In this study the five freedoms not three one is deduced since it is complicated.
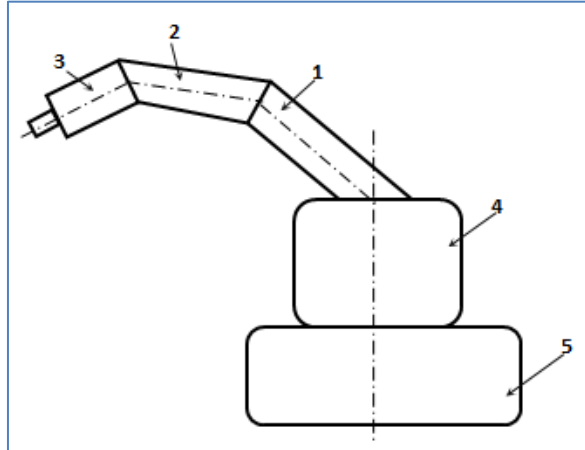

Fig-1: Construction schematic of mechanical arm in series in robot 3-hand part; 2-wrist part;1-arm part; 4-waist part; 5-two crawling wheel
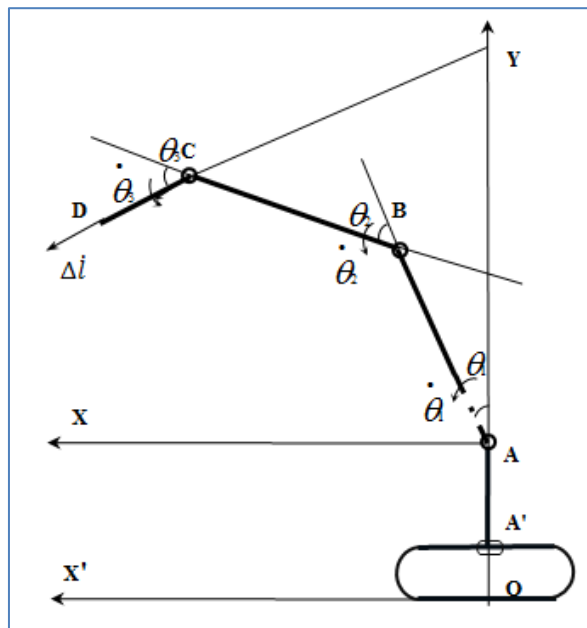
Fig-2: Principle schematic of mechanical arm in series in robot

The system kinetic energy is [1, 3]

$$E_k = \frac{1}{2}\sum_i^n (m_1 v_1^2 + m_2 v_2^2 + m_3 v_3^2) \qquad (1)$$

Here m_i : mass of i component ; J_{si} : rotary inertia of i component relative to center of mass; v_s : center of mass in i component; ω_i : angular velocity in i component; v_1, v_2 and v_3 is 1、2 and 3 velocities respectively.

$$v_{D} = \sqrt{\dot{X}_{D}^{2} + \dot{Y}_{D}^{2}} \tag{2}$$

From Figure 2 it is known that position coordinate below

$$\begin{cases} X_{D} = \vec{l}_{1}\sin\theta_{1} + \vec{l}_{2}\sin(\theta_{1}+\theta_{2}) + \vec{l}_{3}\sin(\theta_{1}+\theta_{3}+\theta_{3}) \\ Y_{D} = (\vec{l}_{1}+\vec{l}_{4})\cos\theta_{1} + (\vec{l}_{2}+\vec{l}_{4})\cos(\theta_{1}+\theta_{2}) + (\vec{l}_{3}+\vec{l}_{4})\cos(\theta_{1}+\theta_{2}+\theta_{3}) \end{cases} \tag{3}$$

Derivating the equations we gain the $\dot{X}_{C}, \dot{Y}_{C}$ and $\dot{X}_{3}$ velocity in hand, $\dot{\theta}_{1}, \dot{\theta}_{2}$ and $\dot{\theta}_{3}$ one in joints. Suppose that the acceleration is $\ddot{\theta}_{1}, \ddot{\theta}_{2}$ and $\ddot{\theta}_{3}$ and the angular acceleration is $\dddot{\omega}_{1}, \dddot{\omega}_{2}$ and $\dddot{\omega}_{3}$ in joints.

$$\begin{cases} \dot{X}_{D} = \dot{\theta}_{1}\vec{l}_{1}\cos\theta_{1} + (\dot{\theta}_{1}+\dot{\theta}_{2})\vec{l}_{2}\cos(\theta_{1}+\theta_{2}) + (\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})\vec{l}_{3}\cos(\theta_{1}+\theta_{2}+\theta_{3}) \\ \dot{Y}_{D} = \dot{\theta}_{1}(\vec{l}_{1}+\vec{l}_{4})\sin\theta_{1} + (\dot{\theta}_{1}+\dot{\theta}_{2})(\vec{l}_{2}+\vec{l}_{4})\sin(\theta_{1}+\theta_{2}) + (\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})(\vec{l}_{3}+\vec{l}_{4})\sin(\theta_{1}+\theta_{2}+\theta_{3}) \end{cases} \tag{4}$$

v_{B}, v_{C} and v_{D} is B、C and D velocities respectively. So D point velocity is

$$v_{D} = \sqrt{\dot{X}_{D}^{2} + \dot{Y}_{D}^{2}} = \sqrt{\begin{array}{l} l_{1}^{2}\dot{\theta}_{1}^{2} + l_{2}^{2}(\dot{\theta}_{1}+\dot{\theta}_{2})^{2} + l_{3}^{2}(\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})^{2} + \dot{\theta}_{1}l_{4}^{2}\sin^{2}\theta_{1}^{2} + l_{4}^{2}(\dot{\theta}_{1}+\dot{\theta}_{2})^{2}\sin^{2}(\theta_{1}+\theta_{2}) \\ + l_{4}^{2}(\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})^{2}l_{4}\sin^{2}(\theta_{1}+\theta_{2}+\theta_{3}) + 2l_{1}l_{3}\dot{\theta}_{1}(\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})\cos(\theta_{1}+\theta_{3}) + \\ 2l_{2}l_{3}(\dot{\theta}_{1}+\dot{\theta}_{2})(\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})\cos\theta_{3} + 2l_{1}l_{4}\dot{\theta}_{1}\sin\theta_{1} + 2l_{2}l_{4}(\dot{\theta}_{1}+\dot{\theta}_{2})\sin(\theta_{1}+\theta_{2}) \\ + 2l_{3}l_{4}(\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})\sin(\theta_{1}+\theta_{2}+\theta_{3}) \end{array}} \tag{5}$$

C point velocity is

$$v_{C} = \sqrt{\dot{X}_{C}^{2} + \dot{Y}_{C}^{2}} = \sqrt{l_{1}^{2}\dot{\theta}_{1}^{2} + l_{2}^{2}(\dot{\theta}_{1}+\dot{\theta}_{2})^{2} - 2l_{1}l_{2}\dot{\theta}_{1}(\dot{\theta}_{1}+\dot{\theta}_{2})\cos\theta_{2}} \tag{6}$$

$$v_{B} = \vec{l}_{1}\dot{\theta}_{1} \tag{7}$$

Substituting two equations above to equation below

$$E_{K} = \frac{1}{2}\vec{l}_{1}(\vec{l}_{1}+\vec{l}_{4}+\vec{l}_{5})(m_{1}+m_{2}+m_{3})\theta_{1}^{2} + \frac{1}{2}\vec{l}_{2}(\vec{l}_{2}+\vec{l}_{4}+\vec{l}_{5})m_{2}(\theta_{1}+\theta_{2})^{2} + \frac{1}{2}\vec{l}_{2}(\vec{l}_{2}+\vec{l}_{4}+\vec{l}_{5})m_{2}(\dot{\theta}_{1}+\dot{\theta}_{2})^{2}$$
$$+ \frac{1}{2}\vec{l}_{3}(\vec{l}_{3}+\vec{l}_{4}+\vec{l}_{5})m_{3}(\theta_{1}+\theta_{2}+\theta_{3})^{2} + 2\vec{l}_{4}^{2}m_{3}\dot{\theta}_{1}\sin^{2}\theta_{2} + \vec{l}_{4}^{2}m_{3}\dot{\theta}_{1}(\dot{\theta}_{1}+\dot{\theta}_{2})^{2}\sin^{2}(\theta_{1}+\theta_{2}) + \vec{l}_{4}^{2}m_{3}(\dot{\theta}_{1}+\dot{\theta}_{2}$$
$$+ \dot{\theta}_{3})^{2}\sin^{2}(\theta_{1}+\theta_{2}+\theta_{3}) + 2\vec{l}_{1}\vec{l}_{2}m_{2}\dot{\theta}_{1}(\dot{\theta}_{1}+\dot{\theta}_{2})\cos\theta_{2} + \vec{l}_{1}\vec{l}_{2}m_{3}\dot{\theta}_{1}(\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})\cos(\theta_{1}+\theta_{2}) + \vec{l}_{2}\vec{l}_{3}m_{3}(\dot{\theta}_{1}$$
$$+ \dot{\theta}_{2})(\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})\cos\theta_{3} + \frac{1}{2}(\vec{l}_{4}+\vec{l}_{5})(m_{1}+m_{2}+m_{3})\theta_{1}^{2} + \frac{1}{2}(\vec{l}_{4}+\vec{l}_{5})m_{2}(\theta_{1}+\theta_{2})^{2} + \frac{1}{2}(\vec{l}_{4}+\vec{l}_{5})m_{2}(\dot{\theta}_{1}+ \tag{8}$$
$$\dot{\theta}_{2})^{2} + 2\vec{l}_{1}\vec{l}_{4}m_{3}\dot{\theta}_{1}\sin(\theta_{1}+\theta_{2}) + 2\vec{l}_{1}\vec{l}_{4}m_{3}(\dot{\theta}_{1}+\dot{\theta}_{2})\sin(\theta_{1}+\theta_{2}) + 2\vec{l}_{3}\vec{l}_{4}m_{3}(\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})\sin(\theta_{1}+\theta_{2}+\theta_{3})$$

Here

$$\frac{\partial E_{K}}{\partial\dot{\theta}_{1}} = (\dot{\theta}_{1}+\dot{\theta}_{2})\vec{l}_{2}m_{2} + 2\vec{l}_{4}^{2}m_{3}\sin^{2}\theta_{2} + 2(\dot{\theta}_{1}+\dot{\theta}_{2})^{2}\vec{l}_{4}^{2}m_{3}\sin^{2}(\theta_{1}+\theta_{2}) + 2 \tag{9}$$

$$\dot{\theta}_{1}(\dot{\theta}_{1}+\dot{\theta}_{2})\vec{l}_{4}^{2}m_{3}\sin^{2}(\theta_{1}+\theta_{2}) + 2\vec{l}_{4}m_{3}\sin^{2}(\theta_{1}+\theta_{2}+\theta_{3}) + 2(\dot{\theta}_{1}+\dot{\theta}_{2})\vec{l}_{1}\vec{l}_{2}$$

$$m_{2}\cos\theta_{2} + 2\dot{\theta}_{1}\vec{l}_{1}\vec{l}_{2}m_{2}\cos\theta_{2} + \dot{\theta}_{1}\vec{l}_{1}\vec{l}_{2}m_{3}\cos(\theta_{1}+\theta_{2}) + \vec{l}_{1}\vec{l}_{2}m_{3}(\dot{\theta}_{1}+\dot{\theta}_{2}+$$

$$\dot{\theta}_{3})\cos(\theta_{1}+\theta_{2}+\theta_{3}) + \vec{l}_{2}m_{3}(\dot{\theta}_{1}+\dot{\theta}_{2})\cos\theta_{3} + \vec{l}_{2}\vec{l}_{3}m_{3}(\dot{\theta}_{1}+\dot{\theta}_{2}+\dot{\theta}_{3})\cos\theta_{3}$$

$$+ 2\vec{l}_{1}\vec{l}_{4}m_{3}\sin(\theta_{1}+\theta_{2}) + 2\vec{l}_{1}\vec{l}_{4}m_{3}\sin(\theta_{1}+\theta_{2}) + 2\vec{l}_{1}\vec{l}_{4}m_{3}\cos(\theta_{1}+\theta_{2}+\theta_{3})$$

$$\frac{\partial E_K}{\partial \dot{\theta}_2} = \vec{l}_2 m_2(\dot{\theta}_1 + \dot{\theta}_2) + \vec{l}_4 m_3(\dot{\theta}_1 + \dot{\theta}_2)^2 \sin^2(\theta_1 + \theta_2) + 2\vec{l}_4 m_3 \dot{\theta}_1(\dot{\theta}_1 + \dot{\theta}_2)\sin$$

$$^2(\theta_1 + \theta_2) + 2\vec{l}_4 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)\sin^2(\theta_1 + \theta_2) + 2\vec{l}_1 \vec{l}_2 m_2 \dot{\theta}_1 \cos\theta_2 + \vec{l}_1 \vec{l}_2 m_2$$

$$(\dot{\theta}_1 + \dot{\theta}_2)\cos\theta_2 + \vec{l}_2 \vec{l}_3 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_2) + \cos(\theta_1 + \theta_2) + \vec{l}_2 \vec{l}_3 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)$$

$$\cos\theta_3 + \vec{l}_2 \vec{l}_3 m_3(\dot{\theta}_1 + \dot{\theta}_2)\cos\theta_3 + 2\vec{l}_1 \vec{l}_4 m_3 \sin(\theta_1 + \theta_2) + 2\vec{l}_1 \vec{l}_4 m_3 \sin(\theta_1 + \theta_2$$

$$+ \theta_3)$$

(10)

$$\frac{\partial E_K}{\partial \dot{\theta}_3} = \vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1 \cos(\theta_1 + \theta_2 + \theta_3) + 2\vec{l}_4 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)\sin^2(\theta_1 + \theta_2 +$$

$$\theta_3) + \vec{l}_1 \vec{l}_2 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)\cos(\theta_1 + \theta_2) + \vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1 \cos(\theta_1 + \theta_2) + \vec{l}_2 \vec{l}_3 m$$

$$_3(\dot{\theta}_1 + \dot{\theta}_2)\cos\theta_3 + \vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1 \cos(\theta_1 + \theta_2) + \vec{l}_2 \vec{l}_3 m_3(\dot{\theta}_1 + \dot{\theta}_3)\cos\theta_3 + 2\vec{l}_1 \vec{l}_4$$

$$m_3 \cos(\theta_1 + \theta_2 + \theta_3)$$

(11)

And

$$\frac{d}{dt}\left(\frac{\partial E_K}{\partial \dot{\theta}_1}\right) = \vec{l}_2 m_2(\ddot{\theta}_1 + \ddot{\theta}_2) + 4(\ddot{\theta}_1 + \ddot{\theta}_2)\dot{\theta}_2 \vec{l}_1 \vec{l}_2 m_2 \sin\theta_2 cos\theta_2 + 4(\ddot{\theta}_1$$

(12)

$$+ \ddot{\theta}_2)\vec{l}_4 m_3 \sin^2(\theta_1 + \theta_2) + 4(\dot{\theta}_1 + \dot{\theta}_2)^3 \vec{l}_4 m_3 \cos(\theta_1 + \theta_2) + 2(\dot{\theta}_1 + \dot{\theta}_2)\vec{l}_4$$

$$m_3 \sin^2(\theta_1 + \theta_2) + 4(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)\vec{l}_4 m_3 \sin(\theta_1 + \theta_2 + \theta_3) - 2\dot{\theta}^2 \vec{l}_1 \vec{l}_2 m_2 \sin\theta_2 - 2$$

$$(\dot{\theta}_1 + \dot{\theta}_2)\dot{\theta}_2 \vec{l}_1 \vec{l}_2 m_2 \sin\theta_1 + 2\ddot{\theta}\vec{l}_1 \vec{l}_2 m_2 \cos\theta_2 - 2\dot{\theta}^2 \vec{l}_1 \vec{l}_2 m_2 \sin\theta_2 + \ddot{\theta}\vec{l}_1 \vec{l}_2 m_3$$

$$\cos(\theta_1 + \theta_2) - \dot{\theta}_1 \vec{l}_1 \vec{l}_2 m_3(\dot{\theta}_1 + \dot{\theta}_2)\sin(\theta_1 + \theta_2) + \vec{l}_2 m_3(\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3)\cos(\theta_1 + \theta_2)$$

$$+ \vec{l}_2 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)(\dot{\theta}_1 + \dot{\theta}_2)\cos(\theta_1 + \theta_2) + \vec{l}_2 m_3(\ddot{\theta}_1 + \ddot{\theta}_2)\cos\theta_3 + \vec{l}_2 m_3(\dot{\theta}_1 + \dot{\theta}_2)$$

$$\dot{\theta}_3 \cos\theta_3 + \vec{l}_1 \vec{l}_2 m_3(\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3)\cos\theta_3 + \vec{l}_2 \vec{l}_3 m_3(\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3)\cos\theta_3 + \vec{l}_2 \vec{l}_3 m_3$$

$$(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)\dot{\theta}_3 + 4(\ddot{\theta}_1 + \ddot{\theta}_2)\vec{l}_1 \vec{l}_4 m_3 \cos(\theta_1 + \theta_2) + 2(\dot{\theta}_1 + \dot{\theta}_2)^3 \vec{l}_1 \vec{l}_4 m_3 \cos(\theta_1 + \theta_2)$$

$$- 2(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)\vec{l}_1 \vec{l}_4 m_3 \sin(\theta_1 + \theta_2 + \theta_3)$$

$$\frac{d}{dt}\left(\frac{\partial E_K}{\partial \dot{\theta}_2}\right) = \vec{l}_2 m_2(\ddot{\theta}_2 + \ddot{\theta}_1) + 2\vec{l}_4 m_3(\dot{\theta}_1 + \dot{\theta}_2)(\ddot{\theta}_2 + \ddot{\theta}_1)\sin^2(\theta_1 + \theta_2) - 4\vec{l}_4 m_3(\dot{\theta}_1$$

(13)

$$+ \dot{\theta}_2)^2(\ddot{\theta}_2 + \ddot{\theta}_1)\sin(\theta_1 + \theta_2)\cos(\theta_1 + \theta_2) + 2\vec{l}_4 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)(\dot{\theta}_1 + \dot{\theta}_2)\sin^2(\theta_1$$

$$+ \theta_2) + 2\vec{l}_4 m_3(\ddot{\theta}_1 + \ddot{\theta}_2)\sin^2(\theta_1 + \theta_2) - 4\vec{l}_4 m_3 \dot{\theta}_1(\dot{\theta}_1 + \dot{\theta}_2)^2 \sin(\theta_1 + \theta_2)\cos(\theta_1 +$$

$$\theta_2) + 2\vec{l}_1 \vec{l}_2 m_3 \ddot{\theta}_1 \cos\theta_2 + 2\vec{l}_1 \vec{l}_2 m_2 \dot{\theta}_1 \dot{\theta}_2 \cos\theta_2 + \vec{l}_1 \vec{l}_2 m_3(\ddot{\theta}_1 + \ddot{\theta}_2)\cos(\theta_1 + \theta_2)$$

$$- \vec{l}_1 \vec{l}_2 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)(\dot{\theta}_1 + \dot{\theta}_2)\sin(\theta_1 + \theta_2) + \vec{l}_1 \vec{l}_2 m_3(\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3)\cos\theta_1 - \vec{l}_1 \vec{l}_2$$

$$m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)\dot{\theta}_1 \sin\theta_1 + \vec{l}_2 \vec{l}_3 m_3(\ddot{\theta}_1 + \ddot{\theta}_2 + \ddot{\theta}_3)\cos\theta_3 + 2\vec{l}_1 \vec{l}_4 m_3(\dot{\theta}_1 + \dot{\theta}_2)\cos(\theta_1$$

$$+ \theta_2) + 2\vec{l}_1 \vec{l}_4 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)\cos(\theta_1 + \theta_2) + 2\vec{l}_1 \vec{l}_4 m_3(\dot{\theta}_1 + \dot{\theta}_2 + \dot{\theta}_3)\cos(\theta_1 + \theta_2 + \theta_3)$$

$$\frac{d}{dt}\left(\frac{\partial E_K}{\partial \dot{\theta}_3}\right) = \vec{l}_1 \vec{l}_2 m_3 \ddot{\theta}_1(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3) + 2\vec{l}_4 m_3(\ddot{\theta}_1+\ddot{\theta}_2+\ddot{\theta}_3)\sin^2(\theta_1+\theta_2+\theta_3) + \qquad (14)$$

$$4\vec{l}_4 m_3(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)^2 \sin(\theta_1+\theta_2+\theta_3)\cos(\theta_1+\theta_2+\theta_3) - \vec{l}_1 \vec{l}_2 m_3(\ddot{\theta}_1+\ddot{\theta}_2+\ddot{\theta}_3)($$

$$\dot{\theta}_1+\dot{\theta}_2)\sin(\theta_1+\theta_2) + \vec{l}_1 \vec{l}_2 m_3 \ddot{\theta}_1 \cos(\theta_1+\theta_2) + \vec{l}_1 \vec{l}_2 m_3 \ddot{\theta}_1 \cos(\theta_1+\theta_2) + \vec{l}_3 \vec{l}_2 m_3$$

$$(\ddot{\theta}_1+\ddot{\theta}_3)\cos\theta_3 - \vec{l}_2 \vec{l}_3 m_3(\dot{\theta}_1+\dot{\theta}_3)\dot{\theta}_3 \sin\theta_3 - \vec{l}_1 \vec{l}_4 m_3 \cos(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)$$

$$\frac{\partial E_K}{\partial \theta_1} = \vec{l}_1(\vec{l}_1+\vec{l}_4+\vec{l}_5)(m_1+m_2+m_3)\theta_1 + \vec{l}_2(\vec{l}_3+\vec{l}_4+\vec{l}_5)\,m_2(\theta_1+\theta_2) + \vec{l}_3(\vec{l}_3+\vec{l}_4+\vec{l}_5)\,m_3(\theta_1+\theta_2+\theta_3) \qquad (15)$$

$$+ 2\vec{l}_4 m_3 \dot{\theta}_1(\dot{\theta}_1+\dot{\theta}_2)^2 \sin(\theta_1+\theta_2) - 2\vec{l}_4 m_3 \dot{\theta}_1(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)^2 \sin(\theta_1+\theta_2+\theta_3) - \vec{l}_1 \vec{l}_2 m_2 \dot{\theta}_1(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)\sin$$

$$(\theta_1+\theta_2) + (\vec{l}_4+\vec{l}_5)(m_2+m_2+m_3)\theta_1 + (\vec{l}_4+\vec{l}_5)m_2(\theta_1+\theta_2) + 2\vec{l}_1 \vec{l}_4 m_3(\dot{\theta}_1+\dot{\theta}_2)\cos(\theta_1+\theta_2) + 2\vec{l}_1 \vec{l}_4 m_3$$

$$(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)\cos(\theta_1+\theta_2)$$

$$\frac{\partial E_K}{\partial \theta_2} = \vec{l}_2(\vec{l}_2+\vec{l}_4+\vec{l}_5)\,m_2(\theta_1+\theta_2) + \vec{l}_3(\vec{l}_3+\vec{l}_4+\vec{l}_5)\,m_3(\theta_1+\theta_2+\theta_3) + 4\vec{l}_4 m_3 \dot{\theta}_1 \sin\theta_2 + 2\vec{l}_4 m_3 \dot{\theta}_1(\dot{\theta}_1+\dot{\theta}_2)^2 \sin$$

$$(\theta_1+\theta_2) + 2\vec{l}_4 m_3 \dot{\theta}_1(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)^2 \sin(\theta_1+\theta_2+\theta_3) - 2\vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1(\dot{\theta}_1+\dot{\theta}_2)\sin\theta_2 - 2\vec{l}_1 \vec{l}_2 m_3 \dot{\theta}_1(\dot{\theta}_1+\dot{\theta}_2)\sin\theta_2 - (\vec{l}_4$$

$$+\vec{l}_5)m_3 \dot{\theta}_1(\theta_1+\theta_2) + 2\vec{l}_1 \vec{l}_4 m_3 \dot{\theta}_1(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)\cos(\theta_1+\theta_2) - (\vec{l}_4+\vec{l}_5)m_3 \dot{\theta}_1(\theta_1+\theta_2) + 2\vec{l}_1 \vec{l}_4 m_3 \dot{\theta}_1 \cos(\theta_1+\theta_2) +$$

$$2\vec{l}_3 \vec{l}_4 m_3(\dot{\theta}_1+\dot{\theta}_1+\dot{\theta}_2)\cos(\theta_1+\theta_2+\theta_3)$$

(16)

$$\frac{\partial E_K}{\partial \theta_3} = \vec{l}_3(\vec{l}_3+\vec{l}_4+\vec{l}_5)(\theta_1+\theta_2+\theta_3) - 2\vec{l}_4 m_3(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)^2 sin(\theta_1+\theta_2+\theta_3) - \vec{l}_2 \vec{l}_3 m_3(\dot{\theta}_1+\dot{\theta}_2) \qquad (17)$$

$$(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)\,sin\theta_3 - 2\vec{l}_3 \vec{l}_4 m_3(\dot{\theta}_1+\dot{\theta}_2+\dot{\theta}_3)\cos(\theta_1+\theta_2+\theta_3)$$

potential energy of System

$$E_P = (\vec{l}_1+\vec{l}_4)\,m_1 g\cos\theta_1 + (\vec{l}_2+\vec{l}_4)\,m_2 g\cos(\theta_1+\theta_2) + (\vec{l}_3+\vec{l}_4)\,m_3 g\cos(\theta_1+\theta_2+\theta_3) \qquad (18)$$

$$\frac{\partial E_P}{\partial \theta_1} = \vec{l}_1 \vec{l}_4 m_1 g \dot{\theta}_1 \sin\theta_1 \qquad (19)$$

$$\frac{\partial E_P}{\partial \theta_2} = \vec{l}_2 \vec{l}_4 m_2 g \dot{\theta}_2 \sin(\theta_1+\theta_2)$$

$$\frac{\partial E_P}{\partial \theta_3} = \vec{l}_3 \vec{l}_4 m_3 g \dot{\theta}_3 \sin(\theta_1+\theta_2+\theta_3)$$

Substituting Lagrange equation below（10）for above equations

Lagrange equation is

$$\frac{d}{dt}\left(\frac{\partial E_K}{\partial \dot{q}_i}\right) - \frac{\partial E_K}{\partial q_i} + \frac{\partial E_P}{\partial q_i} = F_i, \ (i=1,2,,...,n) \qquad (20)$$

Here E_K is kinetic of system;

E_P is potential energy of system;

q_i is generalized coordinate, it is a group of independent parameters that can define mechanical system movement;

F_i is generalized force, when q_i is a angular displacement it a torque, when q_i is linear displacement it a force;

n is system generalized coordinate.

System generalized force

Supposed that Fk(k=1,2,..,m) and Mj(j=1,2,..,n) is force and torque acting on system. Its power is

$$P = \sum_{k=1}^{m}(F_k v_k \cos\alpha_k) + \sum_{j=1}^{n}(\pm M_j \omega_j) \qquad (21)$$

Here ωj: angular velocity acting on component with Mj;
    vk: the velocity in force Fk point of action; (the syntropy +, reverse direction -)
    ak: angle between Fk and vk
When generalized coordinates is φ angular displacement generalized force=equivalent torque Me.

$$\delta W_2 = \sum_{k=1}^{m}(F_k \delta v_k \cos\alpha_k) + \sum_{j=1}^{n}(\pm M_j \delta\omega_j) \qquad (22)$$

Here a_κ is zero; $F_\kappa = 200N$; $v_\kappa = 0.2\sim0.3m/s$; $\omega_j =$; $20\sim30°/s$ $M_j = 20\sim30Nm$. $\delta\varphi_j$ is virtual angular displacement; δs_k is virtual displacement.

Supposing that

$$\delta s_\kappa = \frac{\partial s_\kappa}{\partial q_1}\delta q_1 + \frac{\partial s_\kappa}{\partial q_2}\delta q_2 \qquad (23)$$

$$\delta\varphi_\kappa = \frac{\partial\varphi_j}{\partial q_1}\delta q_1 + \frac{\partial\varphi_j}{\partial q_2}\delta q_2 \qquad (24)$$

Replace equation below with above two equations

$$\begin{cases} F_1 = \sum_{k=1}^{m}\left[F_k \frac{\partial s_\kappa}{\partial q_1}\cos\alpha_k\right] + \sum_{j=1}^{n}\left[M_j \frac{\partial\varphi_J}{\partial q_1}\right] \\ F_2 = \sum_{k=1}^{m}\left[F_k \frac{\partial s_\kappa}{\partial q_2}\cos\alpha_k\right] + \sum_{j=1}^{n}\left[M_j \frac{\partial\varphi_J}{\partial q_2}\right] \end{cases} \qquad (25)$$

This is generalized force equation.

2. DISCUSSIONS

As seen in Table 1 the parameter in robot arm is listed [6, 7]. Here θ_1, θ_2, θ3 is the arm$_1$, arm$_2$, arm$_3$ angle respectively. l_1, l_2, l_3 is arm length. m_1, m_2, m_3 is arm mass. Number is arm label. According to these parameters the below curves are gained as below in Figure 3 &4. As seen in Figure 3(a~c) the force of arm1 will increase with the angular speed and acceleration increasing that expresses the proportional relation between them fitting to Newton theory well. That says that angular speed raises the acceleration meantime the later raise the force too. They all distributes into sinusoidal continuous wave that forms semiwave with 90º. The force may increase from 15N to 15KN and 18KN with F_3, F_1 and F_2 as seen in Figure 4. Among them F_3 is the least one and F_1 is the biggest one. The effect factor turn is $F_1 > F_2 > F_3$ at the angular acceleration of 20º/s^2. So the F_1 is important one attained 1.8Tons and F_2 is second attains 1.5tons while F_3 is neglected. From these value it is observed that F_1 is prior one to ensure the strength and fatigue life then F_2 is second one to estimate its strength whilst F_3 may be neglected in five freedoms. In contrast to above in Figure 3 in three freedoms the force F_1 is about 18KN ie. 1.8tons which is the biggest need to be checked the strength estimation and then F_3 is 75N and at last F_2 is 16N which are neglected here. The effect turn is $F_1 > F_3 > F_2$.

Table-1: Parameters of robot arms

Items	Value	Item	Value
l1 /m	0.55	$\dot{\theta}_1$ /°/s	30~60
l2 /m	0.5	$\dot{\theta}_2$ /°/s	30~60

l3 /m	0.3	$\dot{\theta}_3 /°/s$	30~60
m1/N	7.7	$\ddot{\theta}_1 /°/s^2$	20
m2/N	6.6	$\ddot{\theta}_2 /°/s^2$	20
m3/N	4.0	$\ddot{\theta}_3 /°/s^2$	20

As seen in Figure 3 the force may increase as arm 1 angle increases whilst it may increase if angular speed increases in three freedoms. Meantime it will decrease if angular acceleration increases in Figure 3(d). The maximum is 18KN in Figure 3(a) if angular speed is 20º/s and acceleration is 20º/s² so this point will be checked to ensure the robotic arm strength. There is big distance to attain 3~5KN between the conditions. The effective factor turn to the force is $F_1 > F_3 > F_2$ in three freedoms.
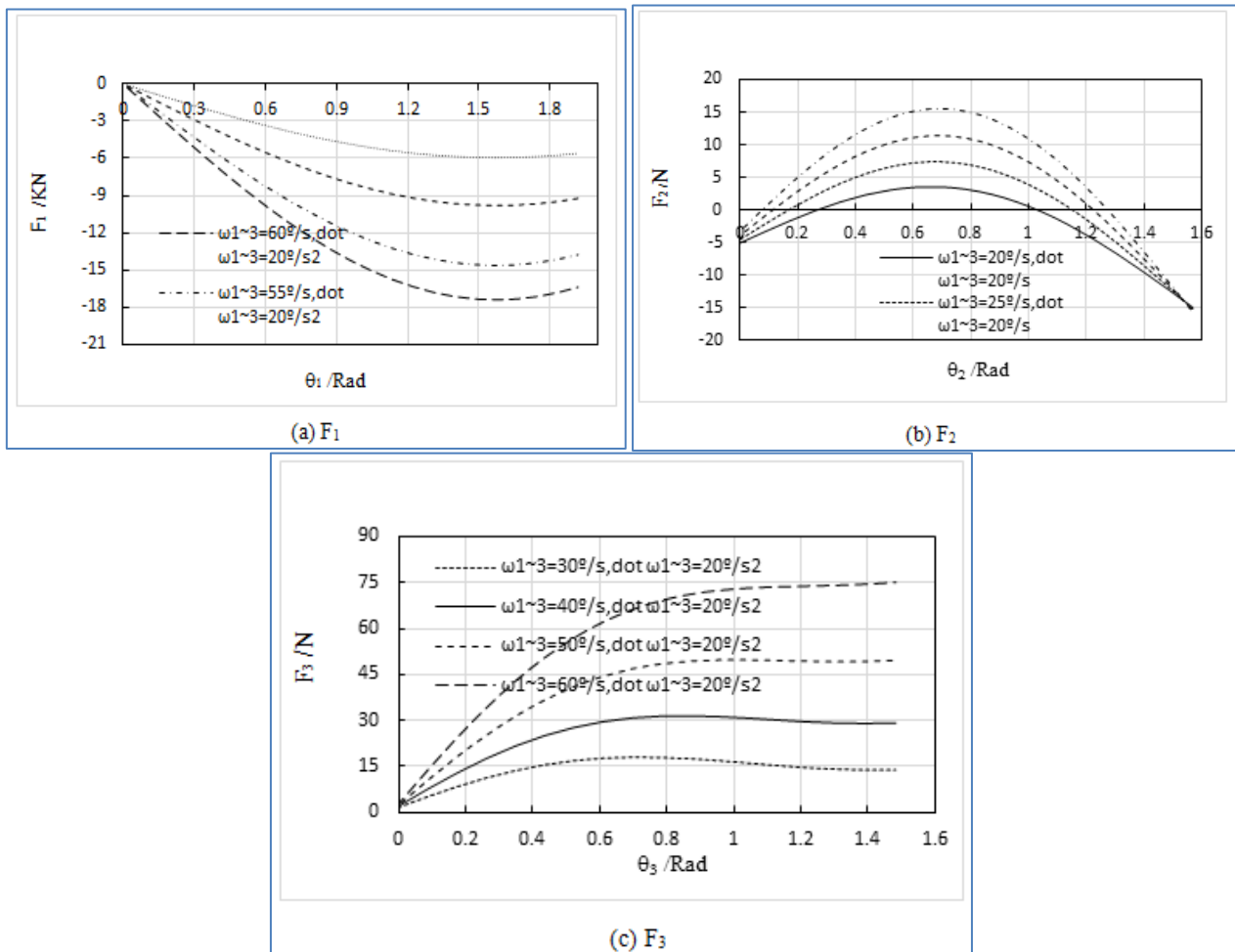

(a) F₁

(b) F₂

(c) F₃

Fig-3: The curve of force and angle with various angular speed and acceleration at angular acceleration of 20º/s2 in three freedoms of robot arm.

In the modeling of five freedoms in movement of robotic arm the kinetic equation is established according to Lagrange formula based on three freedoms robotic arm. It compensates the blank in four freedoms and one impulsion on robot. It is found that the first and second solution is complicated and long the whole equations is concise than the traditional equation. This is a blank in five freedoms which can shorten the whole numerical computation a lot. Referring to the important occasion the kinetic equation will only be computed on three freedoms according to this study.
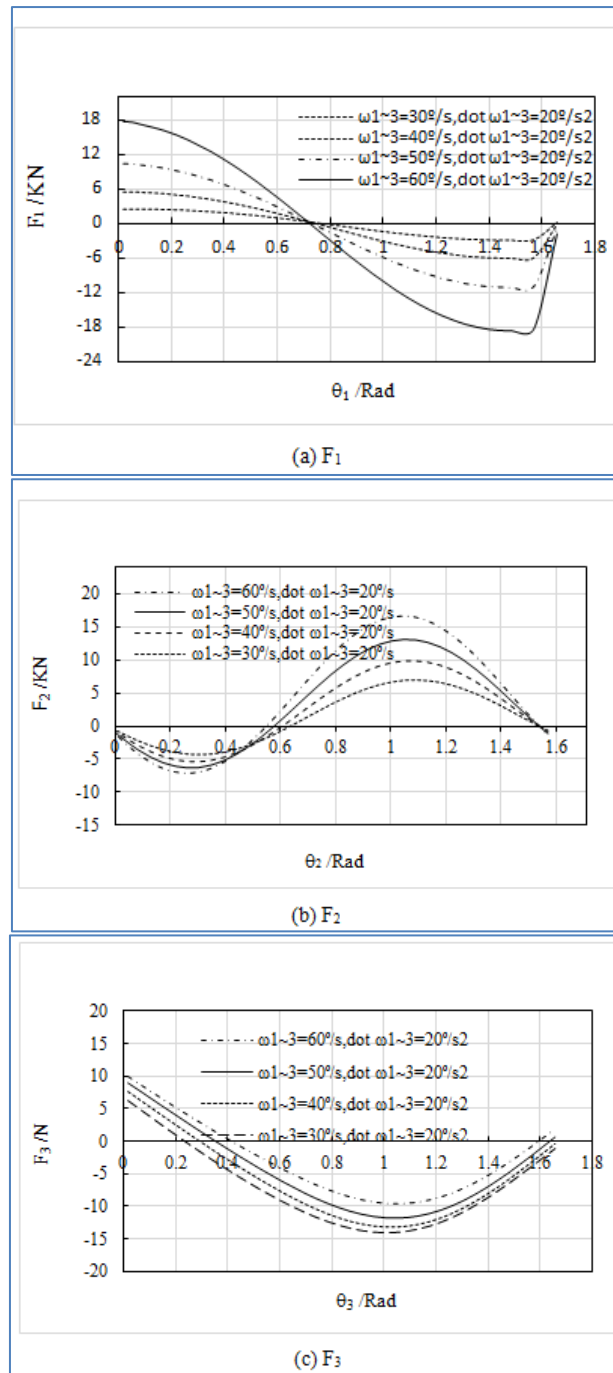
(a) F_1

(b) F_2

(c) F_3

Fig-4: The curve of force and angle with various angular speed and acceleration at angular acceleration of 20º/s2 in five freedoms of robot arm.

It is suggested that the big arm happens when angular speed and acceleration is big. So that the reasonable parameters are chosen to design and estimate their properties is important. Not to choose big angular speed and acceleration is key in order to increase the capability and property that may increase the whole cost as well.

Overview the computation is shorter than the five freedoms traditional one. The solution is easy to use in software like Excel and Origin. The result is satisfactory and precise to be adopted to numerical simulation so the five freedoms method based on three freedoms is feasible.

3. CONCLUSIONS

1. There is big distance to attain 5KN between the conditions. The effective factor turn to the force is $F_1>F_3>F_2$ in three freedoms.

2. The force may increase from 15N to 15KN and 18KN with F_3, F_2 and F_1 in five freedoms. Among them F_3 is the least one and F_1 is the biggest one. The effect factor turn is $F_1 > F_2 > F_3$. so the F_1 and F_2 is important one while F_3 is neglected.

REFERENCES

1. Zhang, C.E. (2008). Machinery dynamics. Higher Educational Press, 96
2. Xiong, Y., Tang, L. (1999). The base of Robotic Technology. Huazhong University of Technology press, 89-90
3. Run, X. (2020). The Dynamic Equation on Hammer with Lagrange in Robotic Arm, *Social Science learning Education Journal, August*, 5(8), 297-300,https://doi. org/10. 15520/sslej.v5i08.2703
4. Li, Doyi. Chen, L., Shang, X., Wang, Z., Wang, W., Yang, X.(2019). Structrue design of pineapple picking manipulator[J], Agricultural Engineering, *9*(2); 1-2
5. Run, X., Boyong, H. (2021). A Simulation between Torque and Angle with Speed on Five Freedoms of Robot Mechanical Arm in Multibody Systems, *Saudi Journal of Civil Engineering, 5*(5); 91-93.DOI: 10.36348/sjce.2021.v05i05.003
6. Pengju, Y. (2012). Base on Dynamics Analysis & Precise Design with Mechanical Arm of Arthritis Rub [D], Master Degree Thesis, Jiangsu University of Technology, 3; 18
7. Zhihua, L.I., Chenjia, W.U. (2020). The Dynamics Solving Method of Flexible Joint Robot Based on Quantized State System[J], *Journal of Mechanical Engineering, 56*(3); 122